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1           **Production of proteases from organic wastes by solid-state fermentation:**  
2                                   **downstream and zero waste strategies**

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4                                   **Short title: Down-stream of proteases produced by SSF**

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23

24 **Abstract**

25 Production of enzymes through solid-state fermentation (SSF) of agro-industrial wastes  
26 reports high productivity with low investment. The extraction of the final product from  
27 the solid waste and solid disposal represent the main cost of the process. In this work,  
28 the complete downstream processes of SSF of two industrial residues for the production  
29 of proteases, soy fibre (SF) and a mixture of hair and sludge (HS), were studied in terms  
30 of activity recovery, using different extraction parameters (extracting solvent, ratio  
31 solid:solvent and extraction mode). Activity after lyophilisation was tested. Solid waste  
32 valorisation after extraction was studied using respiration techniques and biogas  
33 production tests, as part of a zero waste strategy.

34 Results showed a maximum extraction yield of 91% for SF and 121% for HS, both in  
35 agitated mode and distilled water as extraction agent. An average activity recovery of  
36  $95 \pm 6 \%$  and  $94 \pm 6 \%$  for SF and HS respectively was obtained after lyophilisation and  
37 redissolution. To reduce the cost of extraction, a ratio 1:3 w: v solid-solvent in static  
38 mode is advised for SF, and 1:2 w:v extraction ratio in agitated mode for HS, both with  
39 distilled water as extracting agent. Both composting and anaerobic digestion are suitable  
40 techniques for valorisation of the waste material.

41

42 **Keywords:** downstream, extraction, protease, organic wastes, solid-state fermentation,  
43 zero-waste.

44

45

## 46 **Introduction**

47 The use of enzymes in industrial processes is growing every day. They are used, for  
48 example, in detergent manufacturing, bioethanol production and food and beverage  
49 processing. Their use versus traditional chemical processes allows reducing  
50 manufacturing costs and waste generation, also avoiding the need of harsh operational  
51 conditions, as high pressure or temperature (Singh et al. 2016).

52 Two main processes are used to produce enzymes, solid-state fermentation  
53 (SSF) and submerged fermentation. In recent years, the use of SSF has become  
54 outstanding due to its higher yield and the requirement of simpler and smaller  
55 equipment (Kriaa et al. 2016). As substrates, literature provides a wide range of  
56 residues, the most popular being agro-industrial residues, like the coffee pulp waste  
57 used by Kandasamy et al. (2016) to produce protease. These residues are adequate as a  
58 substrate due to their low cost and availability. Besides, several microorganisms have  
59 been reported to produce all types of enzymes when inoculated in sterile conditions on  
60 an adequate substrate (Riyadi et al. 2017, Lizardi-Jiménez and Hernández Martínez,  
61 2017). In fact, the main part of the studies carried out in solid state and submerged  
62 fermentation are focused on the improvement of the production yield by optimizing  
63 fermentation parameters as temperature, particle size, moisture or selecting the right  
64 strain (Sun et al. 2011; Karpe et al. 2015).

65 However, several issues regarding operational conditions still need to be solved  
66 to ensure a successful scale-up of the SSF processes, like overheating problems (Finkler  
67 et al. 2017), or optimization of aeration and agitation modes (Gassara et al. 2013).  
68 Also, since most of the optimal working temperatures of SSF microorganisms are  
69 around 30°C, questions like moisture and temperature are critical in the scale-up of SSF

70 processes. Despite the good yields obtained, SSF is mainly being developed at lab scale  
71 (El-Bakry et al. 2015).

72         Apart from all the technical issues mentioned above, the assessment of the  
73 performance of the entire process at industrial scale, results crucial to determine its  
74 profitability. Activity losses can occur during extraction due to a low contact area  
75 between solid and solvent (Zhang and Sang. 2015), and thus inefficient mass transfer, or  
76 due to stability of the enzyme, which is mainly affected by pH and temperature (Silva et  
77 al. 2014). Storage of the crude extract can also lead to activity losses through time or  
78 during purification (Negi et al. 2011) or lyophilisation stage (Mensink et al. 2017).  
79 Also, the disposal of solid biodegradable residues generated after extraction should be  
80 studied. These residues still contain a considerable amount of biodegradable matter, a  
81 resource to obtain biogas or organic amendments. Despite the relevance of having a  
82 better understanding of downstream and global performance of SSF processes, to our  
83 knowledge, no complete study at pilot scale has been published.

84         Some data obtained at lab scale are provided by Rashid et al. (2013), where  
85 mannose extraction from 0.9 kg of palm kernel cake was studied, finding that soaking  
86 time, nature of solvent, physical state, solid to solvent ratio and number of washes have  
87 great influence on enzyme recovery. Chaithanya et al. (2012) also extracted protease  
88 from fermented bran, finding that the optimum leaching conditions were glycerol and  
89 tap water as solvent, contact time 60 min and agitation at 100 rpm. Both authors  
90 obtained the highest recovery yield when agitation was applied and the solvent was a  
91 mixture of water and glycerol. A solid-solvent ratio of 1:5 (w: v) was also determined as  
92 optimal in both cases. The most influential parameter was the ratio solid-solvent, which  
93 produced the highest difference within the maximum and the minimum activity  
94 recovery in the extraction of protease.

95 In previous works by Abraham et al. (2013) and Abu Yazid et al. (2016), the  
96 listed problems of SSF processes at pilot scale were overcome, developing and  
97 describing robust SSF processes at pilot scale. The operational strategy was based on  
98 allowing the native consortia of microorganisms present in the residue to develop, so  
99 inoculation and sterilization would not be necessary. Protease activity obtained in those  
100 works was remarkably higher than those previously reported and with simpler  
101 operational conditions.

102 Therefore, the aim of this work is to provide a complete picture of the  
103 downstream process of two SSF processes for protease production at pilot scale,  
104 including activity recovery from enzyme extraction, lyophilisation of the crude extract  
105 and activity conservation after dissolving the lyophilised. Downstream processes for  
106 two different wastes, soy fibre waste and cow hair, were studied. Influence of extraction  
107 parameters (w:v ratio, type of solvent and presence/absence of agitation) was studied to  
108 determine the activity recovery obtained with each strategy. Operational conditions  
109 were selected considering their suitability for industrial scale. Regarding the  
110 management of the substrate after extraction, its potential as feedstock for biogas  
111 production was assessed, along with the possible transformation of the solid into an  
112 agricultural organic amendment according to its stability for soil application in a zero  
113 waste strategy.

114

## 115 **Materials and Methods**

116

### 117 **Raw material**

118 Two wastes were assessed for the extraction of protease after SSF, soy fibre (SF), from  
119 a soy beverage manufacturing plant in Castellterçol (Barcelona, Spain), and cow hair,

120 from a local tannery industry located at Igualada (Barcelona, Spain). Cow hair was  
121 mixed with dehydrated sludge from the WWTP (wastewater treatment plant) of  
122 Igualada (Barcelona, Spain) as inoculum for the SSF process in a ratio 1:2 hair: sludge  
123 (w: w) (HS), and moisture was adjusted to 65%. Neither inoculation nor moisture  
124 adjustment was needed for SF as the residue possesses a native population of  
125 microorganisms and adequate water content. In both cases, wood chips from a  
126 composting plant in Manresa (Barcelona) were used as bulking agent in ratio 1:1 (v: v).  
127 SF average particle size is between 800  $\mu\text{m}$  and 0.074  $\mu\text{m}$  while cow hair particle size is  
128 about 1 cm long. 79% in weigh of bulking agent particle size is between 16 mm and  
129 3.15 mm, Soy fibre was stored at  $-20^{\circ}\text{C}$  before the experiments, while fresh sludge and  
130 hair were stored at  $4^{\circ}\text{C}$  due to the structural changes that freezing produces in fresh  
131 sludge. The suitability of these industrial residues as raw materials for protease  
132 production through SSF has been described by Abraham et al. (2013, 2017) and Abu  
133 Yazid et al. (2016), where details of the process and proteases production range are  
134 thoroughly provided.

135

### 136 **SSF Materials and experimental set up**

137 SSF was carried out in 10 L and 50 L (working volume) adiabatic reactors, in order to  
138 minimize environment influence, as described in detail in previous works (Figure 1)  
139 (Maulini-Duran et al. 2014; Puyuelo et al. 2010). Reactors consist in a Dewar-glass with  
140 an outside metallic coverage and an adjusted cap to close the container hermetically.  
141 The inward part of the cap is covered with isolating material. In the bottom of the glass,  
142 a double plastic net was placed to provide support to the fermentable waste, create a  
143 space for lixivates and distribute evenly the inlet air-flow. In the cap, there are three  
144 connexions, two for inlet and outlet gases and the last for a temperature prove. Inside

145 the reactor, a plastic pipe conducts the inlet air to the bottom of the reactor, below the  
146 plastic net. The oxygen content of exhausted gases was measured by an electrochemical  
147 oxygen sensor and data were collected using a personal computer. Data analysis was  
148 carried on by non-commercial software called Sensor. Temperature and air flow were  
149 also measured. A control system for air-flow based in oxygen content in the outlet gases  
150 was used, stablishing an upper and lower set point of 12.5% and 11.5% oxygen content  
151 and variation of volumetric air-flow between values of 300 and 1000 mL min<sup>-1</sup>, assuring  
152 that oxygen was always above 10% in exhaust gases. Reactors capacity (mass) was 3.8  
153 kg of SF and 2.8 kg of HS for 10 L reactors and 17.5 kg of HS and 20 kg of SF for 50 L  
154 reactors, respectively.

155

## 156 **Protease activity recovery - Material and experimental set up**

157

### 158 *Influence of extraction parameters*

159 Extractions were performed to evaluate the recovery of protease activity under different  
160 experimental conditions. 200 g of fermented solid from SSF performed in 10 L and 50  
161 L reactors were used in every extraction. The solid and the solvent were in contact  
162 during one hour under different regimes, at environment temperature, in this case,  
163 around 15 °C, and then the liquid phase centrifuged during 10 minutes at 10000 rpm.  
164 Protease activity of the supernatant was measured and referred to a value considering  
165 the total protease activity produced.

166 To obtain the total protease activity, an extraction in agitated mode at 1:5 solid:  
167 solvent ratio and HCl-Tris (hydroxymethyl aminomethane) buffer pH 8.1 as solvent was  
168 also performed during one hour. The selected ratio was based on Salariato et al. (2010)



169 that extracted polygalacturonase with distilled water at a ratio 1:5. Also, results obtained  
170 in this work from consecutive extractions confirm the accuracy of the choice.

171 The experimental parameters assayed were solvent type, extraction mode and w:  
172 v solid: solvent ratio. The variations of each parameter were:

173 *Solvent type:* Two different solvents were used to perform extractions, distilled  
174 water (DW) and HCl-Tris (hydroxymethyl aminomethane) buffer at pH 8.10  
175 (TB).

176 *Extraction mode:* The extraction modes were three: i) no agitation (static mode),  
177 ii) orbital agitation at 120 rpm, and iii) circulation of the solvent through a  
178 column packed with the waste at  $96 \text{ mL min}^{-1}$ , which resulted in the renewal of  
179 the whole volume of liquid 14 and 7.2 times, for 1:2 w:v and 1:4 w:v extractions  
180 respectively, as added volume of solvent in 1:4 extraction is double than for 1:2.

181 *Waste to solvent ratio (weight: volume):* Assayed ratios of solid: solvent were  
182 1:1, 1:2, 1:3 and 1:4.

183 The different combinations of these tested variables are shown on Table 2.

184 Experimental set up for static and agitated mode consist of a set of glass  
185 containers of different volumes where solvent and solid were placed. Static extraction  
186 was performed introducing the fermented solid and the chosen volume of solvent in a  
187 beaker and waiting for one hour. To obtain the extract in agitated mode, the same  
188 procedure was followed but beakers were placed in a Sony orbital shaker incubator for  
189 an hour at 120 rpm and room temperature.

190 The experimental set up used in liquid circulation extraction was composed of a  
191 peristaltic pump Watson-Marlow 400L2 with variable rotor speed from 2.5 to 50 rpm  
192 and a 0.5 L plastic vessel with two adaptors, one at the top and one at the bottom,  
193 connected by plastic tubes to the pump input and output. Inside the vessel, a device was

194 coupled to let the water fall over the biomass in a drop-shower mode, in order to  
195 achieve a homogenous contact with the solid in a percolation mode. Fermented matter  
196 was placed inside the vessel and solvent added. The flowrate was set up in the pump  
197 and liquid circulation lasted for an hour

198

#### 199 *Number of extraction stages*

200 Enzyme recovery from consecutive stages was assayed performing four consecutive  
201 extractions to the same fermented material. Between extractions, the biomass was  
202 drained to reduce its moisture as much as possible. 1:2 solid: solvent w: v ratio was  
203 chosen for these experiments. Differences between static/agitated mode and TB/DW  
204 were evaluated.

205

#### 206 *Lyophilisation*

207 15 ml of supernatant obtained after centrifugation of the extraction mixture Solid-DW  
208 and Solid-TB were frozen at -80°C and later lyophilized using a Virtis 5L sentry  
209 lyophilizer connected to an Edwards vacuum pump RV5 A653\_01\_903. The protease  
210 activity was measured in the dissolved lyophilized solid and the activity recovery  
211 calculated.

212

#### 213 **Zero waste strategies**

214

#### 215 *Anaerobic digestion - Biogas Potential Test (BPT)*

216 Biomass fermented for the production of protease was tested as feedstock for biogas  
217 production through anaerobic digestion after extraction. Sludge from an anaerobic

218 digester of raw sludge from a municipal WWTP in Sabadell (Barcelona) was used as  
219 inoculum.

220         The methodology used was a modified method of the protocol described by the  
221 German Institute for Standardization and reported by the Ordinance on environmentally  
222 compatible storage of waste from human settlements (2001), detailed by Ponsá et al.  
223 (2010) Inoculum and biomass from SSF were mixed in a feed to inoculum (F/I) ratio of  
224 0.5 for both residues and placed in hermetic closed bottles. Each sample was tested in  
225 triplicate. The ratio F/I was calculated based on the initial amounts of volatile solids  
226 (VS) of substrate and inoculum. According to Ponsá et al. (2010), this ratio is the  
227 optimum to maximize biogas production. The content of volatile solids in fermented SF,  
228 HS and anaerobic inoculum were measured, obtaining a percentage of 26%, 24%, and  
229 1.5%, respectively. A triplicate with only inoculum was also tested as control and its  
230 biogas production subtracted from the sample tests.

231         All the bottles were placed in an incubator Memmert In750 working at 37°C for  
232 21 days. The amount of biogas produced was calculated from the biogas pressure,  
233 measured by an ISE 30A-01-P vacuum switch, temperature and headspace volume. The  
234 bottles were manually agitated before and after measurement, and biogas was  
235 periodically released to avoid overpressure.

236         Representative measures of methane percentage in the biogas were taken at  
237 different days of incubation. Percentage of methane and carbon dioxide were measured  
238 using a gas chromatograph 5890A with a column 17066\_F ParcpackQ (250C), support  
239 100/120, tube 3m 1/8"x 5.5 mm. Initial oven temperature was 70 °C, final oven  
240 temperature was 120°C, determination time was 8 min, injector temperature was 150 °C  
241 and detector temperature was 180°C. Methane peak was detected at 0.8 minutes. 100 µl  
242 of gas sample were required for the analysis.

243

#### 244 *Composting assays*

245 Solid material after SSF and protease extraction was stabilized in order to test its  
246 suitability as soil organic amendment. Experiments were carried out in 50 L and 4.5 L  
247 working volume reactors (Figure 1), for HS and SF respectively. Both reactors have  
248 been previously described (Sayara et al. 2010; Maulini-Duran et al. 2014). 50 L reactor  
249 was a packet bed type reactor, working in almost-adiabatic conditions and made of  
250 steel. Similar to the 10 L reactor, the cover had two connectors for the outlet air and the  
251 temperature probe, at the bottom of the reactor another connector was placed for the  
252 inlet air and also a faucet for lixiviate leaching. The outlet air was conducted through a  
253 water trap at 4 °C, and oxygen content measured by an electrochemical sensor. 4.5 L  
254 reactor is identical to the 10 L reactor described above but in a smaller size. Composting  
255 process was performed with air supplied under OUR control (Puyuelo et al. 2010), a  
256 control system based in an algorithm which assure maximum O<sub>2</sub> consumption during the  
257 experiment. Volumetric flow oscillated between 1300 and 200 mL min<sup>-1</sup> for HS and  
258 between 1000 and 100 mL min<sup>-1</sup> for SF.

259 In the case of HS, a drying stage was required after extraction for moisture  
260 removal, in order to continue the stabilization. During the drying step, the solid was  
261 disposed in thin layer out of the reactor for 24 hours.

262

#### 263 **Analytical methods**

264

##### 265 *Protease activity determination*

266 Protease activity was determined using an adaptation of the Alef and Nannipieri (1995)  
267 method for activity determination in soil (Abraham et al. 2013). According to the

268 methodology, 1 g of soil is mixed in a falcon tube with 5 mL of HCl-Tris buffer pH 8.1,  
269 5 mL of bovine casein salt (2% ) as substrate, covered and incubated for 2 h at 50 °C.  
270 During this time, the protease will break the molecules of casein, releasing peptides and  
271 free amino acids into the media. In this case, 1 g of soil specified in the methodology  
272 was replaced by 1 mL of extract from the SSF and 4 mL of TB were added instead of 5  
273 mL. The conditions for the standard extraction were fixed in a ratio of 1:5 in g of  
274 biomass per mL of HCl-tris buffer pH 8.1, agitation mode and environment  
275 temperature. The extract was centrifuged 10 min at 10000 rpm and the supernatant was  
276 analysed. After the 2 incubation hours, 5 mL of trichloroacetic acid (TCA) (15%) were  
277 added in order to precipitate the non-soluble peptides at this TCA concentration. 1.5 mL  
278 of an alkaline solution and 1 mL of Folin-Ciocalteu reagent (25%) solution were added  
279 to 1 mL of the incubated mixture after centrifugation and then incubated at environment  
280 temperature for 1h, in order to perform a colorimetric determination of the amount of  
281 tyrosine present, using and spectrometer working at 700 nm. L-tyrosine was used as a  
282 standard. So, protease activity was expressed in activity units per gram of dry matter,  
283 being an Activity Unit (U) 1 µg of tyrosine released after 1 hour under incubation  
284 conditions. Calculations were carried out according to Equation 1.

285

$$\text{Protease activity (U g}^{-1}\text{DM)} = \frac{C \ 15 \ V}{\text{DM}} \quad (\text{Eq 1})$$

286

287 Where C is the concentration of tyrosine expressed as µg of tyrosine per ml in the 15 ml  
288 of solution after incubation, 15 is the transformation factor to obtain the concentration  
289 in 1 ml of extract; V is the volume of solvent used in the extraction (ml) and DM (g) is  
290 the dry matter of fermented solid used in the extraction.

291

292 *Activity recovery calculation*

293 Activity recovery was calculated referring the activity obtained in the extraction at  
294 given conditions as a percentage of the standard extraction according to Equation 2.

295

296

$$297 \quad \% \text{ Activity recovery} = \frac{100 \times \text{Protease activity (U g}^{-1} \text{ DM)}}{\text{Standard protease activity (U g}^{-1} \text{ DM)}} \quad (\text{Eq 2})$$

298

299 As the extractions were performed by triplicate, rule of 25% was applied,  
300 discarding the values that differ more than 25% from the average.

301

302 *Chemical oxygen demand (COD)*

303 2 mL of the extract obtained for activity determination with DW as solvent were used to  
304 determine COD with a Lange Kit LCK 514 ranging from 100 to 2000 mg O<sub>2</sub> L<sup>-1</sup> and  
305 COD measures were taken by a Lange Spectrophotometer DR 3900.

306

307 *Dynamic Respirometric Index (DRI)*

308 In this case, respirometric tests were performed on the residues before and after SSF in  
309 order to determine their stability (German Federal Ministry for the Environment, Nature  
310 Conservation and Nuclear Safety, Ordinance on environmentally compatible storage of  
311 waste from human settlements and on biological waste treatment facilities, 2001).

312 A dynamic respirometer following the method described by Adani et al. (2003)  
313 was used. The experimental device was described by Pognani et al. (2011). According  
314 to Gea et al. (2004) the test was carried out at a constant temperature of 37°C. All the  
315 experiments were performed in triplicate. Cumulative oxygen demand, AT<sub>4</sub> (g O<sub>2</sub> kg<sup>-1</sup>

316 dry matter), and Dynamic Respirometric Indices,  $\text{DRI}_{24}$   $\text{DRI}_{1\text{hour}}$  ( $\text{g O}_2 \text{ kg}^{-1}$  dry matter  
317  $\text{h}^{-1}$ ), were calculated (Mejias et al. 2017, Almeida et al. 2015).

318

### 319 *Routine methods*

320 pH was calculated by soaking 10 g of sample in 50 mL of distilled water. After 30 min,  
321 pH value was measured with a pH meter Crison micro pH 2001. Volatile solids,  
322 moisture content, total organic carbon (TOC), total Kjeldahl nitrogen, (TKN) and  
323 Soluble  $\text{N-NH}_4^+$  were measured according to TMECC (The U.S. Department of  
324 Agriculture and The U.S. Composting Council, 2001).

325 TOC (Total Organic Carbon) was determined using an O.I. Analytical Solid  
326 TOC Analyser/Win TOC Solids v3.0, and TKN was measured using a Bloc Digester 6  
327 (with six tubes capacity) (J.P. Selecta S.A., Barcelona, Spain) and a Büchi Distillation  
328 Unit K-355 (Flawil, CH).

329 Fat content (HEM-Hexane extractable material) was measured using a standard  
330 Soxhlet method with n-hexane as organic solvent (The U.S. Environmental Protection  
331 Agency, Method 9071B) (The U.S. Department of Agriculture and The U.S.  
332 Composting Council, 2001).

333

### 334 *Statistics*

335 One-way analysis of variance was performed to compare the mean values of activity  
336 recovery obtained under different experimental conditions. Multiple factor regression,  
337 to obtain a linear equation reflecting the influence of each experimental condition in  
338 activity recovery, was calculated using also activity recovery data. Excel 2010 data tools  
339 was used in both calculations

340

## 341 **Results and Discussion**

342

### 343 **Waste characterization**

344 The results of the characterization of raw materials are summarized in Table 1. As in  
345 this work the objective of SSF was the production of protease, nitrogen-rich substrates  
346 were used. Air Filled Porosity (AFP) of the mixture was measured to ensure a good  
347 aeration of the whole mass. Casciatori et al. (2016) operated with a bed porosity of 0.75  
348 in a mixture of sugarcane bagasse and wheat bran using a packet bed bioreactor.  
349 According to Machado de Castro et al. (2016), a high porosity will ensure the oxygen  
350 transport, but the initial value will change through the process due to degradation of the  
351 support. Porosity seemed to be adequate along the experiment, achieving a good  
352 aeration of the whole sample and no heat loss. Biodegradability was evaluated through  
353 the dynamic respirometric assay. As Table 1 shows, mixtures assayed presented  
354 appropriate initial moisture and porosity, as well as a low C/N ratio. The raw material  
355 chosen as a substrate could be a good inducer of the enzyme produced (Gopalan and  
356 Nampoothiri 2016). So, for protease production using a consortium of microorganism,  
357 the substrate should be a nitrogen-rich one, which means a high content in protein.  
358 Compared to other reported wastes used as substrate for protease production like coffee  
359 pulp, corn cobs (Kandasamy et al. 2016), wheat bran (Meena et al. 2013) or *Jatropha*  
360 *curcas* seed cake (Thanapimmetha et al. 2012), which presented C/N ratios of 18.9  
361 (Eshetu et al. 2013), 36 (Pan-In and Sukasen 2016), 19.49 and 2.46 (Mishra et al. 2016)  
362 respectively, HS and SF present a high content of proteins (nitrogen). Comparing the  
363 reported values of protease production in the mentioned examples, and after  
364 optimization of the experimental conditions in all cases, maximum production  
365 correspond to *Jatropha curcas*, with a range of production near to 1500 U mL<sup>-1</sup>, which



366 was the residue that presented lowest C/N ratio, while the range of production for wheat  
367 bran and the mixture of coffee pulp and corn cobs were 920 U mL<sup>-1</sup> and 582 U mL<sup>-1</sup>  
368 respectively. Although wheat bran presents also a high production value, enrichment  
369 with peptone was carried out previously to the SSF process and only *Jatropha curcas*  
370 was specifically chosen for its high N content, according to the authors. In the present  
371 work, a high protease production was obtained, compared with the examples above,  
372 without any enrichment of the initial mixture, as C/N ratio was already adequate.

373 Material was also biodegradable, as the respirometric values show (Table 4).

374

### 375 **SSF process evolution in 10 L reactors**

376 Figures 2a and 2b show an example of temperature and DRI 1hour (g O<sub>2</sub> kg<sup>-1</sup> DM h<sup>-1</sup>)  
377 profiles obtained in the fermentation process of HS and SF, respectively. The highest  
378 protease activity for HS was always observed in the mesophilic phase after 8 days of  
379 process, while SF protease activity presented its maximum at thermophilic temperatures  
380 after 5 days of fermentation. Maximum activity point was determined in previous  
381 experiments by sampling the reactors periodically and determining the protease activity  
382 for both mixtures. Abraham et al. (2013) found that maximum activity for SF was  
383 observed at the 3<sup>rd</sup> day for a mixture equal to the one used in this work. For this residue,  
384 maximum biological activity concurred with maximum enzymatic activity. On the other  
385 hand, Abraham et al. (2017) found the highest activity value for a mixture of cow hair  
386 and digested sludge at the 14<sup>th</sup> day of fermentation. For the mixture used in this work,  
387 the highest value for protease activity was found in the 8<sup>th</sup> day of fermentation  
388 approximately. Difference with Abraham results can be due to the different inoculum,  
389 as in this work fresh sludge was used. Abu Yazid et al. (2016) characterized the  
390 protease obtained from solid state fermentation of hair and anaerobic sludge

391 determining that the alkaline protease was a serine type in the range between 26 and 100  
392 KDa, and exhibit good stability in a temperature range of 30-50 °C and alkaline pH. In  
393 literature shorter optimum fermentation times are found for protease production through  
394 solid-state fermentation. Kandasamy et al. (2016) found maximum yield of protease  
395 production after 60 h of fermentation, using coffee pulp and corncob as a substrate  
396 inoculating with *Bacillus sp. BT MASC 3*, Pouryafar et al. (2015) determined an  
397 optimum incubation time of 48 h using wheat bran as substrate with *Bacillus*  
398 *licheniformis*. However, in the literature consulted, the SSF process was usually  
399 interrupted after a fixed time, without taking into account the biological activity. So it is  
400 difficult to determine if the maximum production occurred at this time, because no  
401 information about the complete production curve is presented. Also, the highest amount  
402 of solid used in the references found was 25 g. In consequence, temperature control and  
403 oxygen availability was not a limitation of the process. In the present work, SSF was  
404 performed at a pilot scale and this approach requires a complete monitoring of the  
405 process, which makes that highest protease activity is obtained at different times. Thus,  
406 the direct comparison is not possible. High values of DRI 1hour were maintained longer  
407 in the case of SF, which indicates a higher content of rapidly biodegradable material.  
408 These data are in agreement with previous results obtained by Abraham et al. (2013,  
409 2017). The range of protease activity obtained on this work was 6668 to 23541 U g<sup>-1</sup>  
410 DM for HS and 8054 to 33374 U g<sup>-1</sup> DM for SF. For both residues, pH reached values  
411 between 8.0 and 8.8 during the thermophilic phase, and remained in this range until the  
412 end of the process.

413

#### 414 **Protease activity recovery**

415 Factors influencing enzyme extraction from the solid matrix at the point of maximum  
416 protease activity during SSF were evaluated for the two wastes under study. As stated  
417 above, these factors include solvent type, waste: solvent w: v ratio and operation mode  
418 (static, with agitation and recirculation). Table 2 shows the mean and standard deviation  
419 of the protease activity recovery achieved during extraction under the conditions listed  
420 on the same table. Extractions were performed a minimum of three times for each set of  
421 parameters and each residue in agitated and static mode. A duplicate of the extractions  
422 was performed in recirculated mode due to experimental constraints.

423         Maximum activity recovery of  $91 \pm 8$  % for SF was achieved in agitated mode at  
424 1:4 using DW as solvent while a maximum recovery of  $121 \pm 22\%$  was obtained with  
425 the same extraction conditions for HS.

426         The lowest value of activity recovery for SF was obtained at 1:1 w: v with DW  
427 as a solvent and agitated regime. HS presented its minimum at 1:3 w: v extracted with  
428 TB and Static mode.

429         Regarding the mean values of activity recovery of SF, agitated mode presents  
430 approximately 10% more efficiency than static mode. These values represent a higher  
431 recovery in static mode than the results presented by Mrudula and Kokila (2010) for the  
432 extraction of amylase from fermented bran (also a fibrous residue), where a 40% less  
433 recovery in static mode than in agitated mode was reported. However, the difference is  
434 greater for HS residue, which reached 40% difference between agitated and static mode.

435

#### 436 *Solvent type*

437         One factor variance analysis was performed comparing the obtained yields between  
438 experiments differing in one extraction parameter. Results showed, for SF and HS, no  
439 significant difference between recoveries using DW or TB as extractant. Protein

440 solubility depends mostly on polar interactions between the molecules and the solvent,  
441 in some proteins, pH solubility profile presents a minimum value in the isoelectric  
442 region, the value of which depends on the structure of the protein (Hu et al. 2017).  
443 According to Vuong et al. (2016) salt concentration can also affect solubility, either  
444 negatively or positively, as can remove hydrate layers around protein molecules. In this  
445 work, both DW and TB are polar solvents than can be adequate for protease extraction,  
446 but with different initial pH and salinity. However, certain pH can cause deactivation.  
447 Freitas et al. (2013) reported denaturalization of protease from SSF of canola cake at pH  
448 4, so low pH should be avoided. Table 3 show values of pH and conductivity measured  
449 in several extracts. As it can be observed, pH for DW and TB extracts presents similar  
450 results with a maximum pH of 9 and a minimum value of 8.3. Thus, no buffering  
451 properties were needed in the extraction agent to maintain an optimal pH value. pH  
452 achieved is due to the solubilisation of salts and other compounds contained in the solid  
453 matrix, which rise the pH of DW extracts. Differences between both wastes are  
454 reflected in conductivity values, where TB presents higher values due to the Tris salt.  
455 As the extraction ratio decrease, conductivity increase due to higher concentration in  
456 soluble salts from the matrix. During the SSF of SF and HS, proteases were produced  
457 when pH values reached the range of 8-9, thus, these enzymes are expected to be stable  
458 under pH extraction conditions presented in Table 3.

459         According to literature, DW is often used for enzyme extraction with good  
460 yields (Pal and Khanum 2010, Zaslona and Trusek-Howolnia 2015). Karatas et al.  
461 (2013) compared different solvents for the extraction of proteases and  $\alpha$ -amylase from  
462 fermented rice husk, showing tap water the best recovery yield for both enzymes over  
463 HCl-Tris buffer pH 7 and distilled water. In this case, distilled water showed almost  
464 50% less recovery than the buffer. On the other hand, Negi et al. (2011) found as the

465 best solvent for extraction of protease and glucoamylase from wheat bran a solution  
466 containing 10% of glycerol, other solvents assayed were water, ethanol, acetone and  
467 HCl-Tris buffer pH 6.5. Freitas et al. (2013) found that the ideal pH for protease  
468 recovery from fermented canola cake was 7, although they achieved good recoveries at  
469 a range from 5 to 8.

470 According to the results of this work, a solvent which a pH lower than 8.1  
471 should be used, as recovery yield using distilled water was higher, having an initial pH  
472 lower than TB. However, optimum solvent will vary depending on the substrate and the  
473 characteristics of the enzyme produced (Rezaei et al. 2011)

474

#### 475 *Extraction mode*

476 Three different extraction modes were assayed for protease extraction: static extraction  
477 (no agitation), orbital agitation, and recirculation of the solvent at two different  
478 extraction ratios, 1:2 w: v and 1:4 w: v, using a flow of 96 mL/min, which produces 14  
479 times recirculation of the whole volume for 1:2 extractions and 7.2 for 1:4 extractions,  
480 due to the doubled extracting volume. Results for both residues are shown in Table 2.

481 One factor variance test was performed for 1:4 and 1:2 w: v experiments for  
482 both residues. Activity recovery for SF in agitated and static mode was considered  
483 statistically equal in all cases. However, for recirculation mode, differences with  
484 agitated mode were found for 1:4 w: v TB.

485 Sugumaran and Ponnusami (2017) studied the effect of agitation speed in the  
486 extraction of pullulan, a polysaccharide, from two fibrous substrates, cassava bagasse  
487 and palm kernel, reporting increment of 42% and 46% of the recovery obtained at 100  
488 rpm when increasing the agitation speed to 400 rpm and 300 rpm for casaba bagasse  
489 and palm kernel respectively. This difference in recovery depending agitation mode

490 does not agree with the results found in this work. Also, extractions of xylanase from  
491 sorghum straw performed by Adhyaru et al. (2016) showed that in this case  
492 intermedium agitation speed was the optimum and also that interaction between other  
493 extraction parameters like temperature and ration solvent-solid were significant.

494 SF presents very small particle size and once in contact with the solvent losses  
495 its structure allowing good contact solid-solvent. Verdanege et al. (2010) also reported  
496 no influence of the agitation speed in lipase recovery from soybean meal within a range  
497 of 50-150 rpm.

498 When comparing results obtained for HS through one factor variance test,  
499 significant differences are shown in all cases between agitated mode and static  
500 extraction mode. Explanation for these differences is related to the nature of the residue.  
501 Sludge used in HS contains chemical compounds added at the WWTP to produce the  
502 flocculation of the solids and their sedimentation. Nabarlatz et al. (2012) compared  
503 extraction of protease and lipase from two WWTP sludge using stirring and ultra-  
504 sonication, obtaining much better results in almost half of the extraction time for the  
505 second strategy. This shows that the presence of flocks, formed by the chemicals added  
506 to produce the clumping of the solids during water treatment, causes poor contact  
507 liquid-solid.

508 Values of COD for SF and HS extracts, obtained under the same experimental  
509 conditions were 7525 and 3280 mg L<sup>-1</sup> respectively, which indicates a higher  
510 solubilisation of SF material than HS.

511

512 *Volume-weight (solvent-waste) ratio*

513

514 Results of one factor variance test of experiments differing from extraction ratio w: v  
515 showed, for SF, no statistical difference between extractions performed at 1:3 and 1:4  
516 w: v. However, in some cases, significant differences were found between 1:4 and 1:2  
517 w:v extractions and even more significant with 1:1 w:v. When the test was performed  
518 for HS results, there was no difference between recovery at different extraction ratios or  
519 difference appear between 1:4 and 1:3 extraction but not between 1:4 and 1:2 ratios.

520         According to those facts, solubility of protease from SF seems to be high and  
521 related to the equilibrium between concentration of protease in the solid matrix and the  
522 solvent. In the literature, a direct relation between enzyme activity and w: v ratio is  
523 documented. For instance, Adhyaru et al. (2016) assessed the recovery of xylanase from  
524 sorghum straw at different ratios from 8 to 16 mL g<sup>-1</sup> of substrate, locating the  
525 maximum recovery at 12.41 mL g<sup>-1</sup> (5069.20 U g<sup>-1</sup>) when the rest of extraction  
526 parameters had been optimized. Although almost all of the studies performed on this  
527 issue confirm a direct relationship between w:v ratio and activity (Vardanega et al.  
528 2010), the opposite result was reported by Volken et al. (2008) who found a negative  
529 effect of the increase of extraction volume during the extraction of transglutaminase  
530 from industrial fibrous soy residue. Anyway, it must be pointed that although recovery  
531 achieved at higher ratios can be almost total, the obtained extract will present lower  
532 enzyme concentration, requiring extra processes for protease concentration or more  
533 energy during lyophilisation. This fact is not taken into account in most of the works  
534 performed at laboratory scale that do not consider further downstream stages.

535         Linear regression using Excel software was applied to data from Table 2.  
536 Assignment of values to the different extraction parameters in order to perform the  
537 linear regression, as only numbers can be adjusted, was as follow: values of 1 and -1 to  
538 static and agitated mode and also to DW and TB respectively, values of 1, 2, 3, and 4 to

539 extraction ratios of 1:1, 1:2, 1:3 and 1:4, respectively. Recirculation mode results were  
540 excluded from calculations, since experiments in this agitation regime were not  
541 performed with all ratios. Extraction parameters were designated as follows, S for  
542 solvent type, EM for extraction mode, and RA for ratio of extraction w: v. The results  
543 obtained are displayed below for SF (equation 3) and HS (equation 4).

544

$$545 \quad \% \text{ Activity recovery} = 48.9 + 1.7(S) - 3.4(EM) + 9.6(RA) \quad (R^2 = 0.81) \text{ (Eq 3)}$$

$$546 \quad \% \text{ Activity recovery} = 51.3 + 5.2(S) - 18.3(EM) + 9.0(RA) \quad (R^2 = 0.82) \text{ (Eq 4)}$$

547

548 As observed, there is a correlation between the different results, as regression  
549 coefficients are 0.81 and 0.82, considered high for experimental values.

550 SF regression shows the highest coefficient for RA, which means that extraction  
551 ratio has the greater influence in the extraction of protease. However, for HS, the  
552 parameter that presents more relevance is the extraction mode. In both cases, it is clear  
553 that agitated mode will produce the maximum recovery yield.

554 To sum up, the facts that can be deduced from those equations agree with the  
555 results obtained by one factor variance test, indicating that extraction yield will increase  
556 with extraction ratio for SF with little dependence on the agitation mode. When  
557 proteases are extracted from HS, agitation must be applied to achieve maximum activity  
558 recovery, but a lower extraction ratio is allowed.

559

#### 560 *Number of extraction stages*

561 Consecutive extractions were carried out for HS and SF using DW and TB in a ratio of  
562 1:2 w: v with agitation and in static mode. Figure 3 a) and b) shows the percentage of  
563 activity recovery for the consecutive extractions performed on 200 g of fermented solid.



564 As it can be seen for both residues, approximately the 80% of the total activity  
565 recovered is extracted during first and second extraction, leaving a small amount of  
566 protease in the solid matrix. For both residues, the final percentage of activity recovery  
567 is higher for agitated regime. Regarding the total activity recovery after two consecutive  
568 extractions, it is possible to conclude that with 1:5 extraction ratio in agitated mode and  
569 TB as solvent, practically a 100% recovery of the protease contained in the solid matrix  
570 for both residues can be achieved.

571 Ahmed and Mostafa (2013) reported a recovery of 98% of exo-  
572 polygalacturonase produced by solid state fermentation of orange bagasse under  
573 optimum leaching conditions after three washes. However, 70% of the enzyme was  
574 extracted with the first wash. Also, Abd el Aty and Mostafa (2015) Extracted  $\alpha$ -amylase  
575 from pre-treated and fermented potato shells with six consecutive washes at the  
576 optimum extraction parameters, achieving a recovery of 90.3% at the fourth one. In this  
577 case, recovery in the first and second extraction was very similar, approximately a 35%.  
578 Comparing the results obtained for protease, activity recovery yield was higher in both  
579 SF and HS. In view of these results it seems that efficiency recovery of successive  
580 extraction stages may be related to the type of enzyme and specifically studied in  
581 economic terms.

582

### 583 *Lyophilisation process*

584 15 ml of fresh extract were lyophilised and the remaining solid powder dissolved in DW  
585 to its original volume. The activity of that solution was measured and compared to the  
586 fresh extract to determine the activity recovery of the lyophilisation process. The  
587 process was performed by duplicate. Lyophilisation resulted in high yields of activity  
588 recovery, for SF,  $95 \pm 4$  % was recovered as a mean value and  $96 \pm 6$  % for HS extracts.

589 No relation between extraction parameters and activity conservation was observed, as  
590 samples of each set of extraction parameters were assayed. Minimum activity recovered  
591 was  $87 \pm 3$  for HS and 88% for SF. Abu Yazid et al. (2016) reported an activity loss of  
592 21% after lyophilisation of protease extract obtained also from the fermentation of hair  
593 and sludge. During freezing and drying, protein can suffer denaturation, losing its  
594 activity. Bonds between water molecules disappear during drying process, but some  
595 components present the ability to stabilize the protein structure and preserve activity  
596 (Mensink et al. 2017). The same protein in a different matrix can lead to different  
597 activity preservation. Activity losses have been reported by Imamura et al. (2014) for  
598 different proteins after drying in sodium and potassium phosphate buffer. The highest  
599 recovery with no salts addition reached 31%. Thus, lyophilisation in this case results in  
600 low activity losses compared to the results reported, and a possible explanation can be  
601 that no unfolding of the protein is happening during lyophilisation.

602

### 603 **Protein hydrolysis by SSF produced protease**

604 Abu Yazid et al. (2017) described the immobilisation of protease, obtained from the  
605 same residues used in this work, onto functionalized magnetic iron oxide nanoparticles  
606 through covalent binding method, obtaining a retention yield of 96%. Abu Yazid et al.  
607 (2017) also used the immobilized enzymes during at least three cycles for protein  
608 hydrolysis with no loss of activity. With an initial protein amount of 5.2 mg from  
609 casein, the degree of protein hydrolysis achieved was 75% and 50% of the initial  
610 amount of protein for enzymes produced by HS and SF respectively.

611 According to those results, for a 50 L reactor of fermented HS and SF (17.5 kg  
612 and 20 kg respectively), obtaining the maximum activity achieved in this work, 23541  
613 U DM<sup>-1</sup> for HS and 33374 U DM<sup>-1</sup> for SF, it would be possible to hydrolyse 156.6 mg

614 and 238.3 mg of protein from casein bovine with the recovered protease from HS and  
615 SF respectively. For this calculation the immobilized enzyme would be used during 6  
616 cycles, in which initial activity does not diminish until the fourth cycle. Jin et al. (2010),  
617 reported hydrolysis of 2.1 mg of protein from rapeseed meals in one cycle using 1  
618 mL of immobilised protease on ferric nanoparticles solution (8.50 mg/mL), during two  
619 hours incubation at 50°C. Hydrolysis yield in this case was lower (9.86%) compared to  
620 the one reported by Abu Yazid et al. (2017) (75% and 50%). Comparing activity to  
621 commercial products, neutral protease for beer brewing (Food grade) provided by  
622 Creative Enzymes (Creative enzymes) was taken as example. The mentioned product  
623 activity, as manufacturing specifications says is 70000 U/g, being a unit the amount of  
624 enzyme that hydrolyses casein to get 1 µg of tyrosine in 1 min. at 30°C and pH 7.5. Abu  
625 Yazid et al. (2017) was capable of immobilize 45.9 U / mg of ferric nanoparticles (NP)  
626 for HS and 31.9 U / mg nanoparticles (NP) for SF, being a unit (U) the amount of  
627 enzyme that hydrolyses casein to get 1 µg of tyrosine in 1 min. at 50°C and pH 8.1, The  
628 resulted product described by Abu Yazid et al. (2017) will have an activity of 45900 U /  
629 g NP, and being reusable during at least 3 cycles without activity loss, resulted in a  
630 much better yield than the commercial one.

631

### 632 **Zero waste strategies**

633 As described above, the solid residue obtained after extraction was tested as feedstock  
634 for biogas and soil organic amendment production in the framework of a zero waste  
635 strategy.

636

637 *Anaerobic digestion*

638 Biogas potential tests were undertaken to determine the suitability of anaerobic  
639 digestion to treat the solid waste after enzyme extraction. After 21 days, SF replicates  
640 produced 365, 304 and 273 mL of biogas  $\text{g}^{-1}$  VS with a content of approximately 43%  
641 of methane. During the same period of time, HS produced 132 and 111 mL biogas  $\text{g}^{-1}$   
642 VS, with both presenting 40% of methane content. Biogas production in this case was  
643 significantly lower than for SF. This result was expected since HS fermentation lasted 6  
644 more days than SF, so HS was more biodegraded at the point of maximum protease  
645 production and extraction.

646 Kafle et al. (2013) reported biogas potential of different agricultural and animal  
647 wastes like apple waste, bread waste or cutlet fish waste. The values reported ranged  
648 from 508 to 617 biogas  $\text{mL g}^{-1}$  VS, significantly higher than the values reported in this  
649 study, since SF and HS were already partially degraded. Values reported by Ponsá et al.  
650 (2011) of biogas production for organic fraction of municipal solid waste with no  
651 mechanical pre-treatment ( $340 \text{ mL g}^{-1}$  DM) and for municipal solid waste with  
652 mechanical pre-treatment ( $133 \text{ mL g}^{-1}$  DM) are in the range of SF and HS biogas  
653 production values obtained in the present study. No values of biogas production were  
654 found in literature regarding SF and HS before and after SSF and extraction, Merlino et  
655 al. (2012) reported a production approximately of  $590 \text{ Nm}^3 \text{ t}^{-1}$  VS of broken soybean  
656 after 35 days of digestion at  $40 \text{ }^\circ\text{C}$ , with a methane content of approximately a 55%.  
657 That data is barely comparable to biogas production of SF since SF was already a  
658 fermented material and a part of SF volatile solids were lignocellulosic, non-  
659 biodegradable material.

660

661 *Composting process*

662 The stabilization of the solid waste after enzyme extraction under aerobic conditions  
663 was also tested. Composting was evaluated as a valorisation technology to obtain an  
664 organic soil amendment.

665 HS required a drying stage after enzyme extraction and before composting, in  
666 order to decrease its moisture content from 74% to 62%. Before drying, no biological  
667 activity was occurring despite the aeration provided. According to Chen et al. (2012),  
668 excessive water content can hamper the oxygen transfer.

669 For HS, temperatures up to 55°C, required for sanitation were not reached during  
670 composting. This is probably due to the amount of waste in the reactor (17 kg)  
671 compared to industrial scale quantities to which EU regulations apply (European  
672 Commission, Working document, Biological treatment of Biowaste 2nd draft, 2001).  
673 Abu Yazid et al. (2016) also composted a mixture of hair and anaerobic digested sludge  
674 after fermentation and extraction of protease at a 10 L scale for approximately 30 days  
675 without reaching thermophilic temperatures. Onyuka et al. (2013) composted a mixture  
676 of cow hair and soil achieving maximum temperature of 51 °C at a scale of 2 L. In an  
677 industrial scale, it would be expected to reach the required temperature for sanitation, as  
678 heat gradient will increase as scale does (Ge et al. 2017). Table 4 shows  $DRI_{24}$  values of  
679  $2.0 \pm 0.1$  and  $0.61 \pm 0.05$  for initial mixture of HS after SSF and composted product  
680 respectively, indicating that the material becomes stable after composting. This stage  
681 lasted 5 days for HS.

682 In the case of SF, SSF experiments were stopped for enzyme extraction at the 3<sup>rd</sup>  
683 and 5<sup>th</sup> day of process, showing values of average oxygen uptake rate during the last 24  
684 hours ( $OUR_{24}$ ) of 3, 4.5, 9 g O<sub>2</sub> kg<sup>-1</sup> DM h<sup>-1</sup> in thermophilic range. Thus, SF was  
685 clearly a non-stable material at this stage of the process.

686 Composting of SF after SSF and enzyme extraction was carried out in 4.5 L  
687 reactors in duplicate. Both replicates showed an increase of temperature and oxygen  
688 consumption during the first 24h, followed by a fast decrease to environment  
689 temperature. The maximum temperature values reached were 34°C and 42°C  
690 respectively, and maximum OUR<sub>24</sub> values around 5 g O<sub>2</sub> kg<sup>-1</sup> DM h<sup>-1</sup>, but never  
691 reaching the thermophilic range again.

692 After 9 days of composting process, the residue could not be considered stable  
693 as it presented a DRI<sub>24</sub> value of 2.1 ± 0.4 g O<sub>2</sub> kg<sup>-1</sup> DM h<sup>-1</sup> and AT<sub>4</sub> value of 146 ± 27 g  
694 O<sub>2</sub> kg<sup>-1</sup> DM. A longer composting process will be needed, since the decrease of  
695 biological activity is slow.

696 According to Barrena et al. (2009), aerobic and anaerobic indices are closely  
697 related. Values reported for the ratio between DRI<sub>24</sub> and biogas production in liquid  
698 condition and between AT<sub>4</sub> and biogas production at the same condition for different  
699 wastes were 86 and 1.56 respectively. The same ratios were calculated using the values  
700 obtained in this study, giving values of 84 and 1.56 respectively. These numbers agree  
701 with the parameters reported by Barrena et al. (2009).

702

## 703 **Conclusions**

704 In this work a complete assessment of the downstream of SSF processes for the  
705 production of proteases has been performed (Figure 4). Yields of activity recovery in  
706 protease extraction and lyophilisation stages, under a wide variety of conditions, were  
707 calculated. According to the results, extraction ratio of 1:3 for SF is recommended and  
708 agitation mode at extraction ratio 1:2 would be the adequate conditions for HS.  
709 Consecutive extractions in static mode seem an efficient way of obtaining also a good  
710 yield, with no agitation but double extraction time. Economical balance between

711 profitability of the recovered product and water/energy consumption should be  
712 performed. Lyophilisation provides a high activity recovery, around 95% as an average.  
713 It was also observed that as the solubility of the solid matrix increases, the ratio waste:  
714 solvent w: v becomes the most determining factor in the activity recovery yield, while  
715 agitation mode is the key factor when solubility decrease.

716         After enzyme extraction, the use of SF and HS as feedstock for anaerobic  
717 digestion reported relatively high biogas production. Also, HS and SF could be treated  
718 through composting obtaining a stable product.

719

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725

726

## 727 **Conflict of interest**

728

729 On behalf of all authors, the corresponding author states that there is no conflict of  
730 interest.

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## Figure captions

Figure 1. a) 4.5 L and 10 L reactors, b) 50 L reactor

1: 4.5 L and 10 L reactor; 2: 4.5 L and 10 L reactor inside; 3: Mass-flowmeter; 4: Temperature probe; 5: Water trap; 6: O<sub>2</sub> Electrochemical sensor. 7: 50 L reactor; 8: 50 L reactor inside

Figure 2. Temperature (lines) and DRI 1 hour (short-short) profiles obtained in SSF processes a) HS fermentation, b) SF fermentation.

DRI 1h: Dynamic Respirometric Index 1 hour average value

Figure 3. Percentage of activity recovery obtained in consecutive extractions of 200 g of fermented solid at 1:2 w: v ratio a) HS b) SF.

HS: Hair and Sludge; SF: soy fibre; TB: HCl-Tris Buffer (pH = 8.10); DW: Distilled water

Figure 4. Downstream summary.

DRI 1h: Dynamic Respirometric Index 1 hour average value; AT<sub>4</sub>: Cumulative Oxygen Consumption during 4 days; HS: Hair and Sludge; SF: soy fibre; TB: HCl-Tris Buffer (pH = 8.10); DW: Distilled water; VS: Volatile Solids

Table 1: Characterization of wastes and mixtures used as substrates in SSF

Parameters	Hair waste	Sludge	HS	SF
Moisture (% , wb)	67 ± 8	75 ± 2	62.3 ± 0.8	67 ± 8
Organic matter (% , db)	86 ± 1	67	89 ± 1	96 ± 3
pH	9.9 ± 0.8	7.8 ± 0.4	7.6 ± 0.3	6 ± 2
EC (mS cm <sup>-1</sup> )	4.5 ± 0.8	2.3 ± 0.9	3 ± 1	0.9 ± 0.2
Total organic carbon (% , db)	51 ± 9	n.a.	64 ± 3	69 ± 3
Total Kjeldahl Nitrogen (% , db)	10 ± 4	16	7.3 ± 0.5	4.9 ± 0.6
C/N ratio	6 ± 1	3	7.1 ± 0.8	14 ± 1
Fat content – HEM (% , db)	0.9 ± 0.3	n.a.	n.a.	6 ± 2
Air filled porosity (%)	n.a.	n.a.	77 ± 4	74

wb: wet basis. db: dry basis; n.a.: not available; HEM: Hexane extractable material.

HS: Hair waste:sludge (1:2, w.w) and wood chips (1:1, v:v); SF: Soy fibre and wood chips (1:1, v:v).

Values are the average of independent experiments and its standard deviation.

Table 2: Summary of extraction experiments for fermented soy fibre (SF) and fermented cow hair and sludge (HS) (Extraction time: 1h)

% Activity recovery				Extraction parameters		
SF Mean	SF St deviation	HS Mean	HS St deviation	Solvent (S)	Extraction mode (EM)	Ratio W:V (RA)
<b>53</b>	9	<b>71</b>	5	DW	Agitated	1:1
<b>54</b>	10	<b>66</b>	3	TB	Agitated	1:1
<b>55</b>	4	<b>49</b>	8	DW	Static	1:1
<b>55</b>	9	<b>52</b>	4	TB	Static	1:1
<b>83</b>	18	<b>99</b>	16	DW	Agitated	1:2
<b>70</b>	6	<b>93</b>	19	TB	Agitated	1:2
<b>73</b>	12	<b>49</b>	3	DW	Static	1:2
<b>65</b>	8	<b>50</b>	6	TB	Static	1:2
<b>63</b>	6	<b>71</b>	8	DW	Recirculated	1:2
<b>71</b>	2	<b>58</b>	8	TB	Recirculated	1:2
<b>88</b>	20	<b>114</b>	18	DW	Agitated	1:3
<b>85</b>	3	<b>72</b>	9	TB	Agitated	1:3
<b>74</b>	3	<b>62</b>	2	DW	Static	1:3
<b>78</b>	22	<b>44</b>	6	TB	Static	1:3
<b>91</b>	8	<b>121</b>	22	DW	Agitated	1:4
<b>86</b>	3	<b>99</b>	23	TB	Agitated	1:4
<b>79</b>	8	<b>66</b>	11	DW	Static	1:4
<b>77</b>	7	<b>72</b>	3	TB	Static	1:4
<b>76</b>	19	<b>93</b>	21	DW	Recirculated	1:4
<b>72</b>	1	<b>56</b>	12	TB	Recirculated	1:4

DW: Distilled water, TB: HCl – Tris buffer (pH = 8.10), EM: Extraction mode, S: Solvent type, RA:Ratio of extraction w:v



Table 3: pH and conductivity of the extracts

SF (Fermented Soy Fibre)					HS (Fermented Hair + Sludge)				
S	EM	RA	pH	Conductivity (mS/cm)	S	EM	RA	pH	Conductivity (mS/cm)
DW	Agitated	1:1	8.9	6.9	DW	Agitated	1:1	8.7	11.46
DW	Agitated	1:2	8.9	4.7	DW	Agitated	1:2	8.83	7.77
DW	Agitated	1:3	8.9	3.2	DW	Agitated	1:3	8.78	5.83
DW	Agitated	1:4	9.0	2.9	DW	Agitated	1:4	8.77	4.76
DW	Static	1:1	8.5	2.4	DW	Static	1:1	8.79	10.16
DW	Static	1:2	8.7	3.0	DW	Static	1:2	8.82	5.99
DW	Static	1:3	8.7	3.5	DW	Static	1:3	8.81	4.34
DW	Static	1:4	8.6	2.7	DW	Static	1:4	8.85	4.32
TB	Agitated	1:1	8.6 ± 0.2	7.5 ± 0.5	TB	Agitated	1:1	8.69	12.04
TB	Agitated	1:2	8.5 ± 0.1	6.1 ± 0.7	TB	Agitated	1:2	8.6	8.76
			8.5 ±						
TB	Agitated	1:3	0.04	5.2 ± 0.2	TB	Agitated	1:3	8.5	7.09
TB	Agitated	1:4	8.4 ± 0.04	4.7 ± 0.4	TB	Agitated	1:4	8.51	6.67
					TB	Static	1:1	8.58	12.55
					TB	Static	1:2	8.54	8.35
					TB	Static	1:3	8.37	5.83
					TB	Static	1:4	8.31	5.09

DW (distilled water): pH: 7.81, Conductivity: 1.86 (mS/cm); TB (HCl – Tris buffer): pH: 8.1, Conductivity: 2.48 (mS/cm)

Table 4. Results of respirometric assays. Final SSF values are initial composting values.

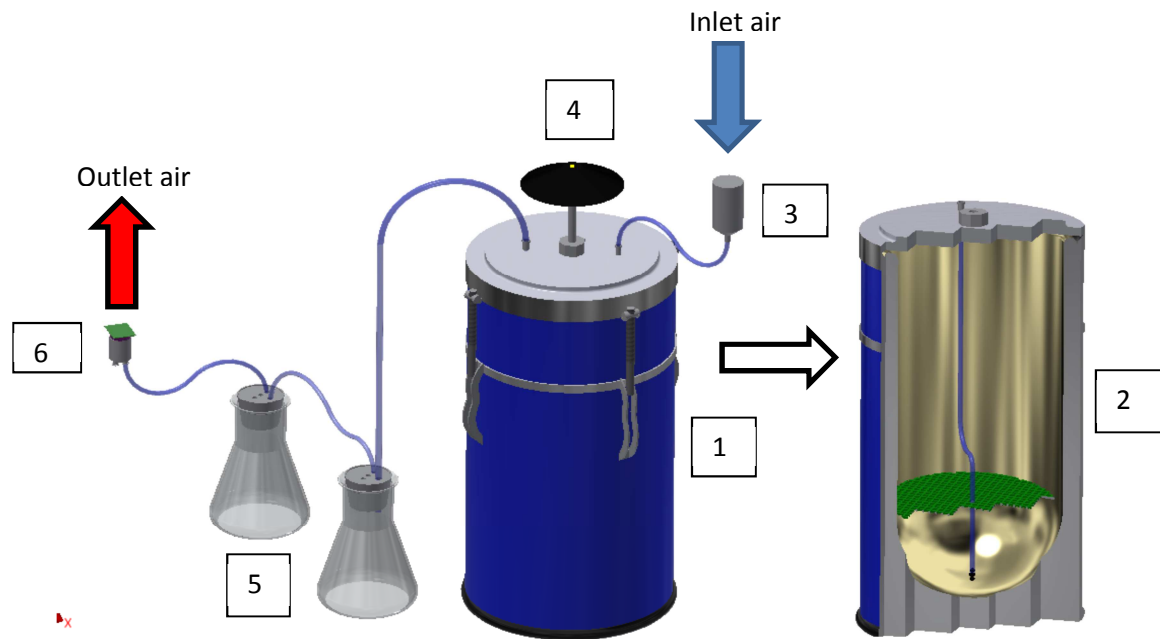
Residue	Solid State Fermentation				Composting	
	Initial AT <sub>4</sub> (g O <sub>2</sub> kg <sup>-1</sup> DM)	Final AT <sub>4</sub> (g O <sub>2</sub> kg <sup>-1</sup> DM)	Initial DRI <sub>24</sub> (g O <sub>2</sub> kg <sup>-1</sup> DM h <sup>-1</sup> )	Final DRI <sub>24</sub> (g O <sub>2</sub> kg <sup>-1</sup> DM h <sup>-1</sup> )	Final AT <sub>4</sub> (g O <sub>2</sub> kg <sup>-1</sup> DM)	Final DRI <sub>24</sub> (g O <sub>2</sub> kg <sup>-1</sup> DM h <sup>-1</sup> )
SF	326 ± 98	185 ± 48	5 ± 2	3 ± 1	146 ± 27	2.1 ± 0.4
HS	113 ± 11	61 ± 6	2.0 ± 0.1	1.0 ± 0.1	48 ± 4	0.61 ± 0.05

AT<sub>4</sub>: Accumulated O<sub>2</sub> consumption after 4 days; DRI<sub>24</sub>: dynamic respirometric index based on 24 hours of maximum O<sub>2</sub> consumption.

Values are the average of independent experiments.

Figure 1

a)



b)

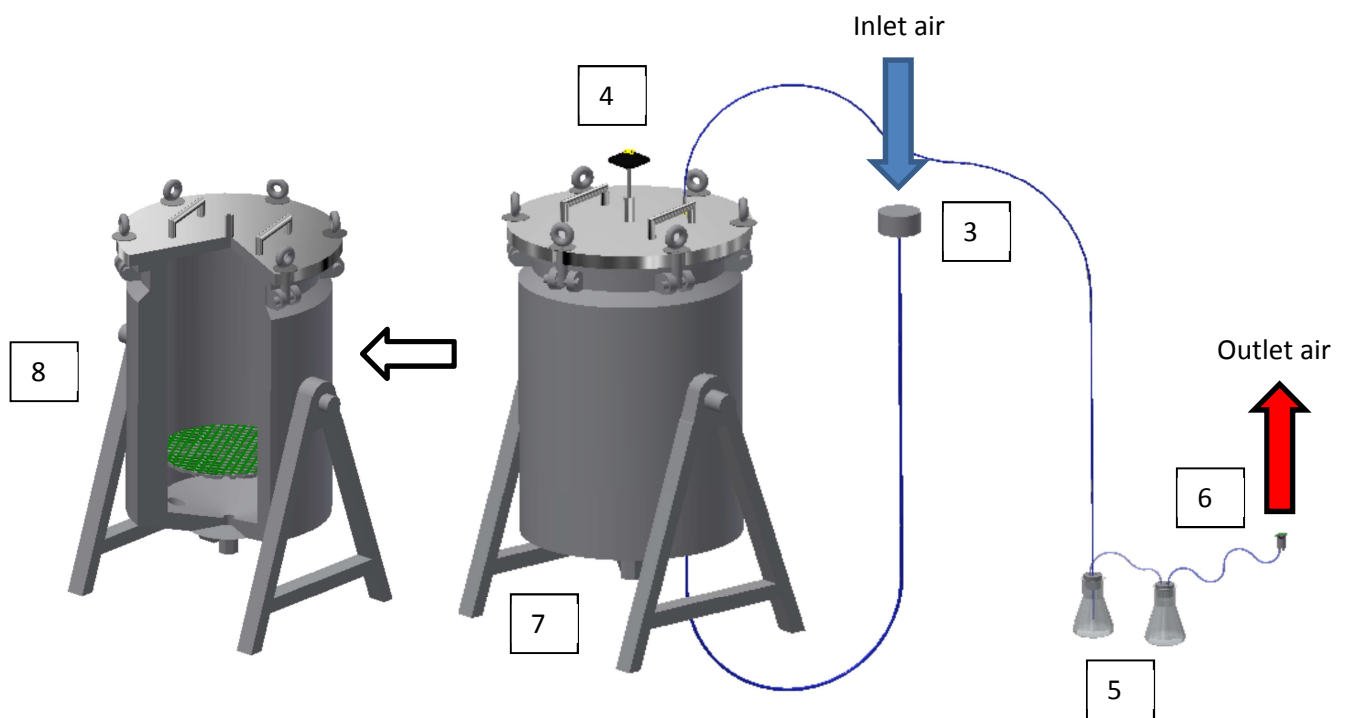
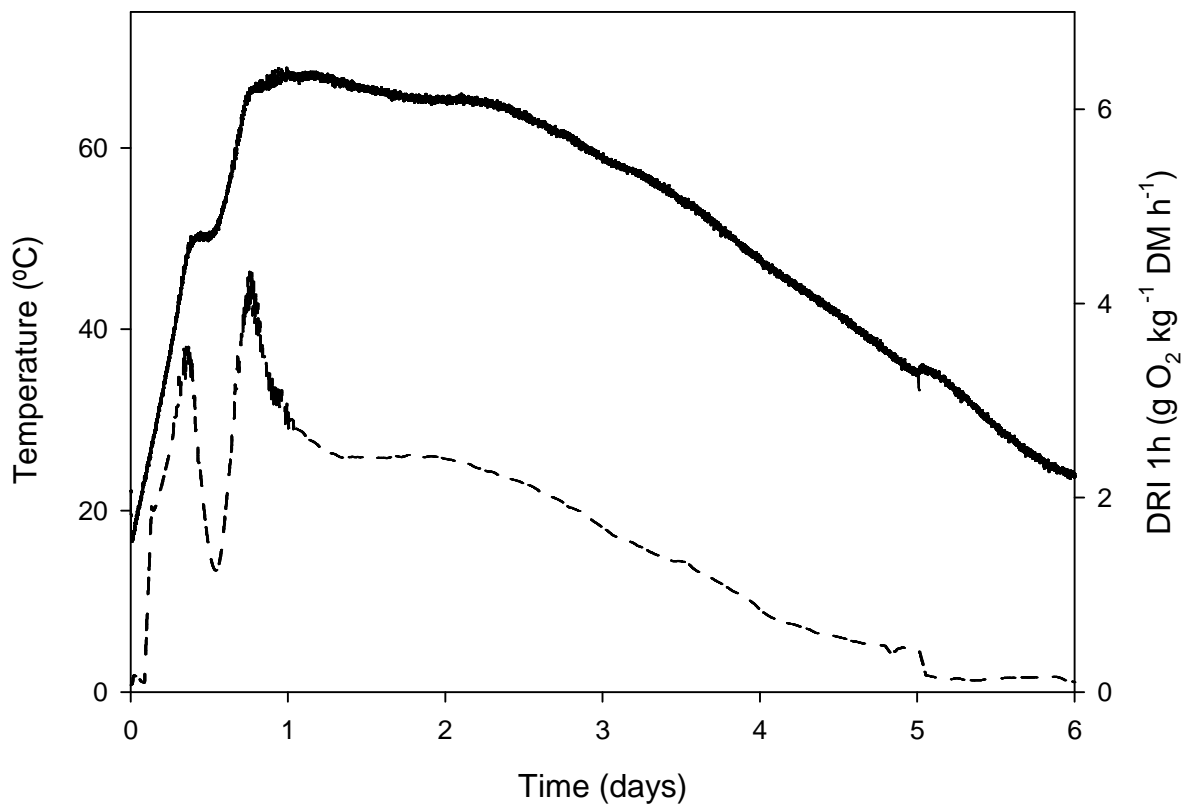


Figure 2

a)



b)

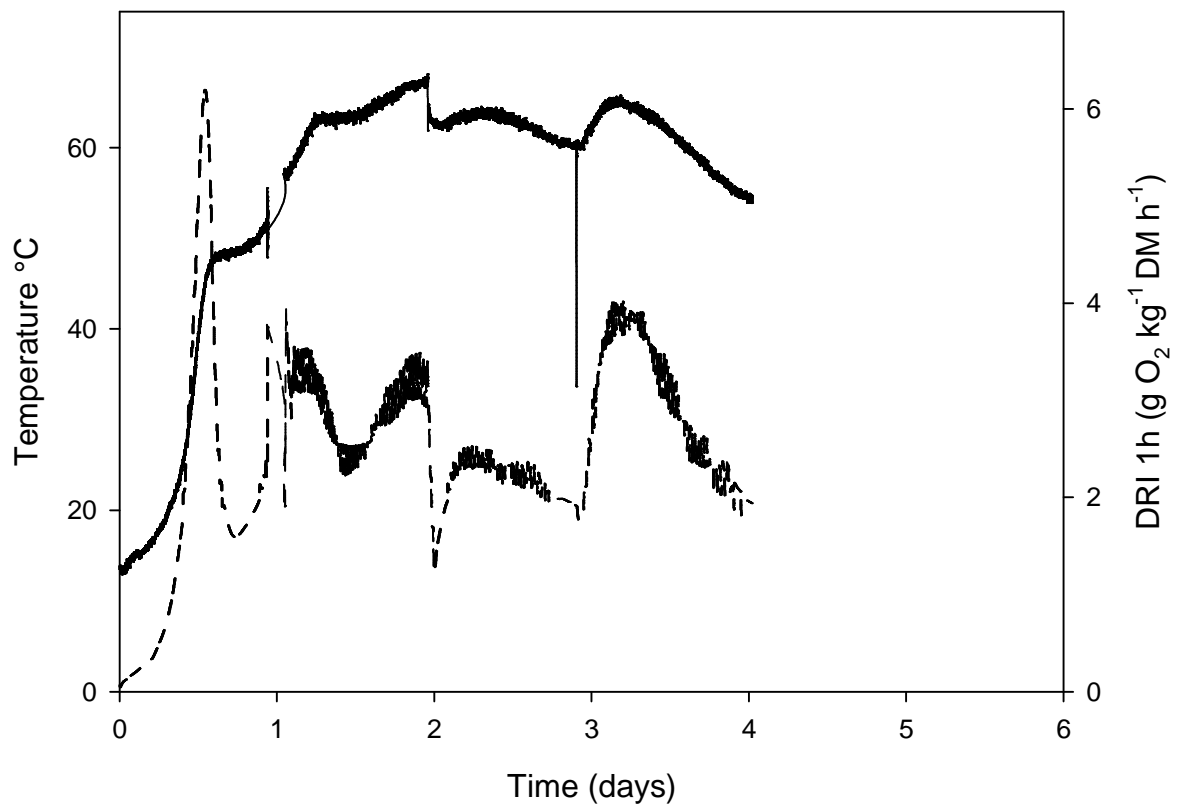


Figure 3

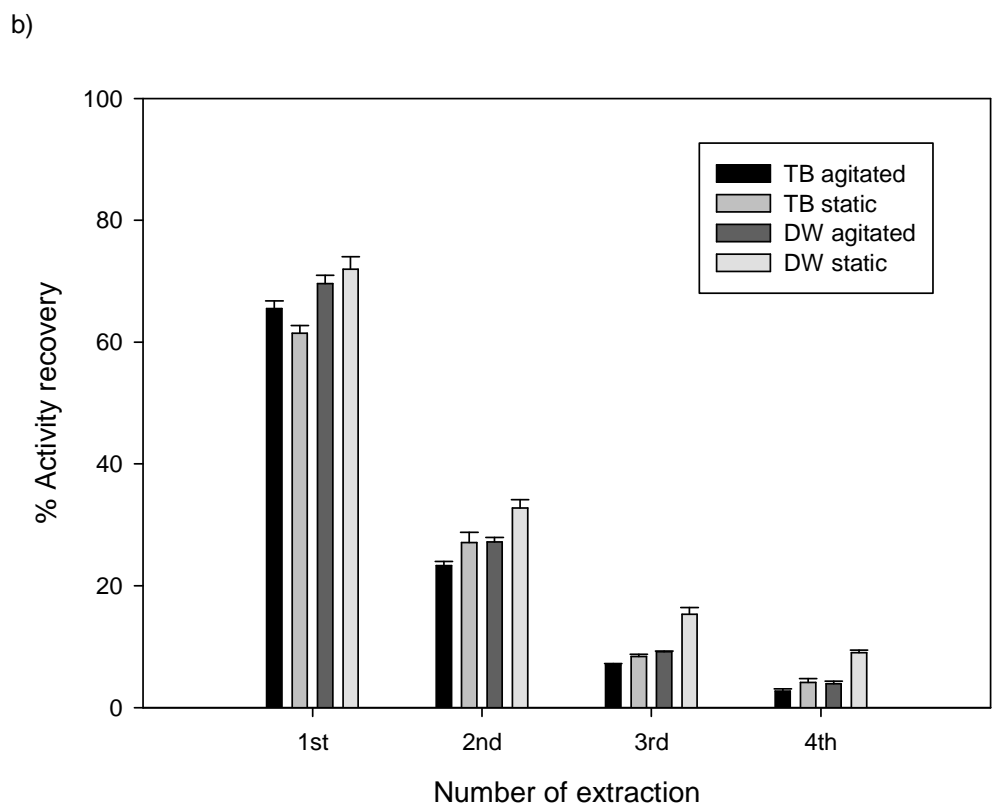
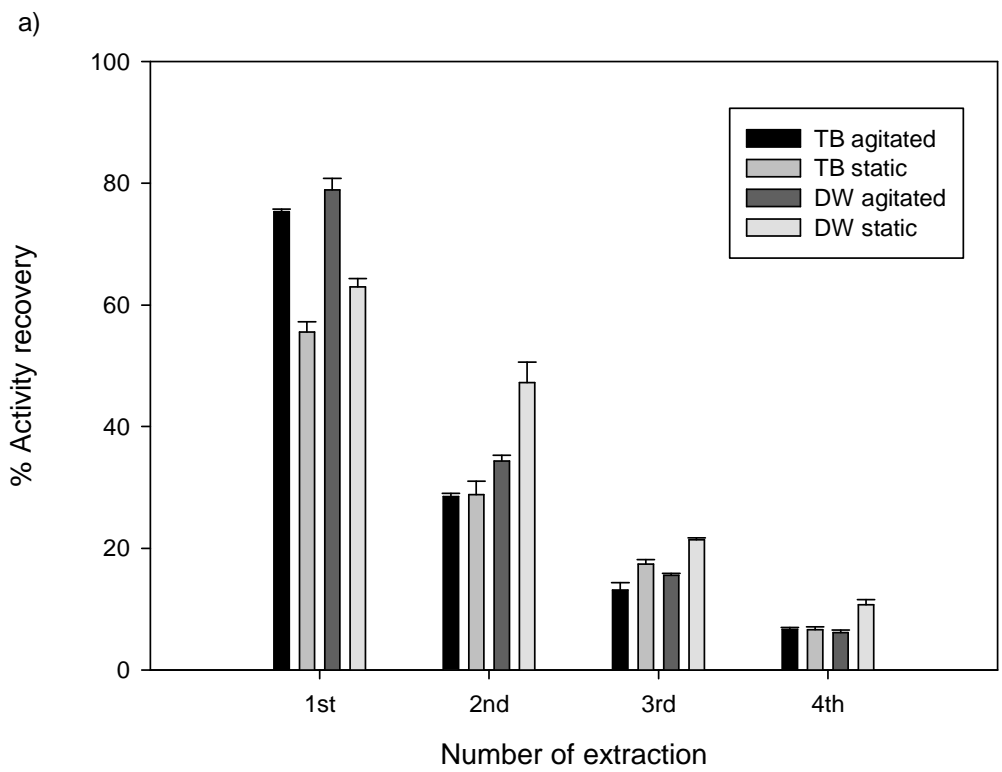


Figure 4

